

Solutions to TSE110 Analog Filters 160321

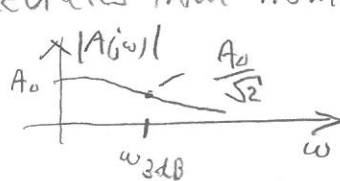
a) Linear $a_1 x_1(t) + a_2 x_2(t) \rightarrow a_1 y_1(t) + a_2 y_2(t)$ if $x(t) \rightarrow y(t)$
 Time-invariant $x(t-t_0) \rightarrow y(t-t_0)$

b) LP: 2 zeros at $s = \infty$, BP: one zero at $s = 0$
 HP: 2 zeros at $s = 0$, one zero at $s = \infty$

c) Overdesigned (higher filter order) due to band edge symmetries and the same attenuation in both passbands / stopbands
 BS BP

d) Low sensitivity \Rightarrow small variations in $H(j\omega)$ when component values deviate from nominal values

e) $\omega_z = A_0 \cdot \omega_{3dB}$



$$A(j\omega) = \frac{A_0}{1 + j\frac{\omega}{\omega_{3dB}}}$$

Approx. the bandwidth of the filter in which the opamp is used
 max

2) Filter order (nomogram $\frac{\omega_s}{\omega_z} = 2$) $N = 5$

Table C0515θ, $30 \leq \theta \leq 36$ Select $\theta = 33$ (for ex)

Normalized poles:

- 0,6046827
- 0,1335634 ± j 1,0725098
- 0,4279530 ± j 0,7336827

Normalized zeros

- ± j 1,9153952
- ± j 2,9552877
- one at ∞

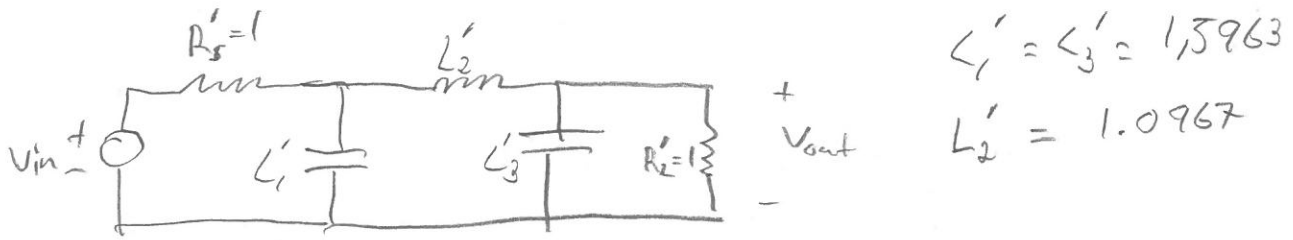
Denormalize, mult by $\omega_c \Rightarrow$

poles = $-3,7993334 \times 10^6$
 $(-0,8392036 \pm j 6,7387778) \times 10^6$
 $(-2,6889080 \pm j 4,6098644) \times 10^6$

zeros $\pm j 1,2034783 \times 10^7$
 $\pm j 1,8568620 \times 10^7$
 one at ∞

3) $\frac{LP \text{ prototype}}{R_c} = \frac{\omega_I^2}{\omega_c} \left\{ \text{use } \omega_I^2 = \omega_c \right\} = 1, \quad R_s = \frac{\omega_I^2}{\omega_s} = \frac{\omega_c}{\omega_s} = 5$

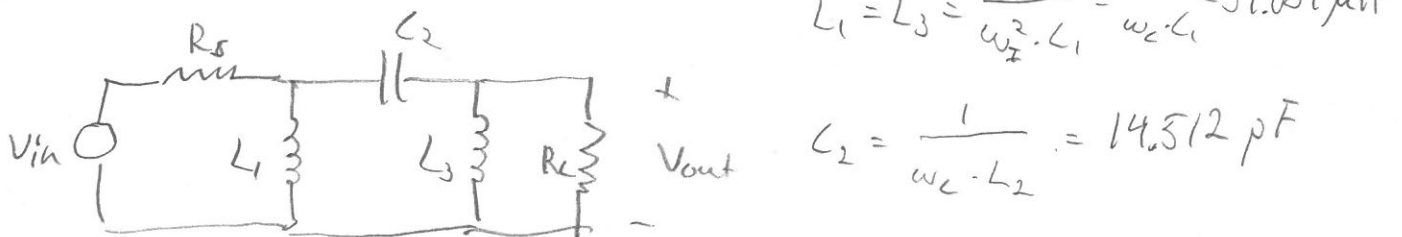
\Rightarrow Filter order $N=3$



Denormalize with $R_c=1, R=R_s=R_L=2k\Omega \Rightarrow$

$C_1 = C_3 = \frac{C'_1}{R_c \cdot R} = 0.79815 \text{ mF}, \quad L_2 = L'_2 \cdot \frac{R}{R_c} = 2.1934 \text{ kH}$

LP \rightarrow HP



4) a) BP: $a=c=0, b \neq 0, BS: a \neq 0, c \neq 0, b=0$

b) $H(j\omega) = \frac{e}{(j\omega)^2 + d \cdot j\omega + e}, \quad |H(j\omega)| = \frac{|e|}{\sqrt{(e-\omega^2)^2 + d^2\omega^2}}$

$\frac{\partial |H(j\omega)|}{\partial \omega} = |e| \cdot \frac{2(e-\omega^2) \cdot -2\omega + 2d^2\omega}{((e-\omega^2)^2 + d^2\omega^2)^{1.5}} = 0$ when $\omega=0$ here not the sol. / we want

and when $-4(e-\omega^2) + 2d^2 = 0 \Leftrightarrow \omega^2 = e - \frac{d^2}{2} \Leftrightarrow \omega = \sqrt{e - \frac{d^2}{2}}$
 ($\omega = -\sqrt{e - \frac{d^2}{2}}, |H(j\omega)| = |H(-j\omega)|$)

$\therefore \omega_{\text{peak}} = \sqrt{e - \frac{d^2}{2}}$

with $e=10, d=1: \omega_{\text{peak}} = \sqrt{10 - \frac{1}{2}} \approx 3.082207$

$\Rightarrow |H(j\omega_{\text{peak}})| \approx 3.2025$

(Note: with $e=r_p^2, d=-2\sigma_p = \frac{r_p}{Q}: \omega_{\text{peak}} = r_p \sqrt{1 - \frac{1}{2Q^2}}$)

$$5/a) \underline{BP}: s + \frac{\omega_T^2}{s} - p = 0 \Leftrightarrow s^2 - ps + \omega_T^2 = 0 \Rightarrow$$

$$\text{poles at } \frac{p}{2} \pm \sqrt{\frac{p^2}{4} - \omega_T^2} = \left(p=4, \omega_T^2=4 \cdot 7^2 \right) = -2 \pm j \sqrt{4 \cdot 7^2 - 4}$$

$$\approx -2 \pm j 3.9564$$

$$\text{zeros at } s=0 \text{ \& } s=\infty \quad \left(s + \frac{\omega_T^2}{s} - \infty = 0 \right)$$

$$\underline{BS}: \frac{\omega_T^2}{s + \frac{\omega_T^2}{s}} - p = 0 \Leftrightarrow \frac{\omega_T^2 \cdot s}{s^2 + \omega_T^2} - p = 0$$

$$\Leftrightarrow p \cdot s^2 - \omega_T^2 s + \omega_T^2 \cdot p = 0 \Leftrightarrow s^2 - \frac{\omega_T^2}{p} s + \omega_T^2 = 0$$

$$\Rightarrow \text{poles at } \frac{\omega_T^2}{2p} \pm \sqrt{\left(\frac{\omega_T^2}{2p}\right)^2 - \omega_T^2} \approx 4.9348 \pm j 3.8892$$

$$\text{zeros at } s = \pm j \omega_T \quad (s^2 + \omega_T^2 = 0) = \pm j 2.77 \approx \pm j 6.2832$$

$$b) \frac{1}{sL} \xrightarrow{BS} \frac{1}{\frac{\omega_T^2 \cdot C}{s + \frac{\omega_T^2}{s}}} = \frac{s + \frac{\omega_T^2}{s}}{\omega_T^2 \cdot C} = \frac{s}{\omega_T^2 C} + \frac{1}{sC}$$

$$= sL + \frac{1}{sC}, \quad L = \frac{1}{\omega_T^2 \cdot C}$$

$$6/a) \begin{pmatrix} V_1 \\ I_1 \end{pmatrix} = \begin{pmatrix} A & B \\ C & D \end{pmatrix} \begin{pmatrix} V_2 \\ -I_2 \end{pmatrix} \text{ and } V_2 = -I_2 \cdot Z_2 \Leftrightarrow -I_2 = V_2 / Z_2$$

$$\Rightarrow Z_{in}(s) = \frac{V_1(s)}{I_1(s)} = \frac{A(s)V_2(s) + B(s)V_2(s)/Z_2(s)}{C(s)V_2(s) + D(s)V_2(s)/Z_2(s)} = \frac{A(s) + B(s)/Z_2(s)}{C(s) + D(s)/Z_2(s)}$$

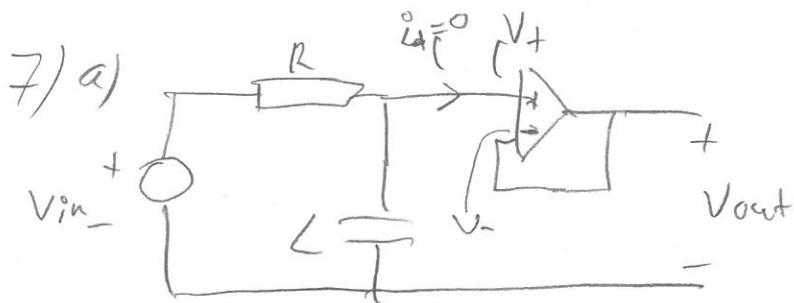
$$\left(\text{Alt.} = \frac{A(s)Z_2(s) + B(s)}{C(s)Z_2(s) + D(s)} \right)$$

$$b) Z_2(s) = \frac{10^8}{s}, \quad A, B, C, D \text{ const.} \Rightarrow \frac{V_1(s)}{I_1(s)} = \frac{A + B \cdot s \cdot 10^{-8}}{C + D \cdot s \cdot 10^8}$$

$$= \text{Desired: } 10^{-4} s \quad \text{Select } A = D = 0 \Rightarrow$$

$$\frac{V_1(s)}{I_1(s)} = \frac{B}{C} \cdot s \cdot 10^{-8} \quad \text{select } \frac{B}{C} = 10^4 \Rightarrow \frac{V_1(s)}{I_1(s)} = 10^{-4} s$$

$$\text{For ex. } B = 10^4 \\ C = 1$$



$$V_{out}(s) = A(s) (V_+(s) - V_-(s)) \quad (1)$$

$$V_+(s) \stackrel{\uparrow}{=} V_{in}(s) \cdot \frac{1/sC}{R + 1/sC} = V_{in}(s) \cdot \frac{1}{1 + sRC} \quad (2)$$

volt. div. since $i_+ = 0$, i.e., $i_R = i_C$

$$V_-(s) = V_{out}(s) \quad (3)$$

$$(1) - (3) \Rightarrow V_{out}(s) = A(s) (V_{in}(s) \cdot H_1(s) - V_{out}(s))$$

$$\Rightarrow H(s) = \frac{V_{out}(s)}{V_{in}(s)} = \frac{H_1(s) \cdot A(s)}{1 + A(s)} = H_1(s) H_2(s)$$

$$b) H_1(j\omega) = \frac{1}{1 + j\omega RC}, \quad \omega_{3dB}: \omega RC = 1 \Rightarrow \omega_{3dB} = \frac{1}{RC} = 1000 \text{ rad/s}$$

$$H_2(j\omega) = \frac{A(j\omega)}{1 + A(j\omega)} = \frac{\frac{A_0}{1 + j\omega/\omega_0}}{1 + \frac{A_0}{1 + j\omega/\omega_0}} = \frac{A_0}{1 + A_0 + j\omega/\omega_0}$$

$$\omega_{3dB}: \frac{\omega}{\omega_0} = 1 + A_0 \Rightarrow \omega_{3dB} = \omega_0 (1 + A_0) \approx \omega_0 A_0 = 2\pi \cdot 10^6 \text{ rad/s}$$

$H(j\omega)$: ω_{3dB} approx the same as for $H_1(j\omega)$ since the bandwidth of $H_2(j\omega)$ much larger

