

Exam in TSEI10 Filters

Exam code:	TEN1	
Date:	2017-06-08	Time: 14–18
Place:	U1	
Examiner:	Håkan Johansson	
Department:	ISY	
Allowed aids:	Pocket calculator Wanhammar: Tables and formulas for analog and digital filters Söderkvist: Formler och Tabeller Ingelstam, Rönngren, Sjöberg: Tefyma Ekbohm: Tabeller och Formler NT Nordling: Physics Handbook for Science and Engineering Strid: Formler och Lexikon Mathematical tables	
Number of tasks:	7	
Grading:	Maximum 70 points, 30 points required to pass the exam. Note that a motivation/solution is required to get the maximal number of points for a problem. Note that 10, 8, 6, 4, or 2 points obtained at the seminars means that you do not have to solve Problem 1, 1(a)-(d), 1(a)-(c), 1(a)-(b), or 1(a), respectively.	
Solutions:	Will be published no later than three days after the exam at http://www.commsys.isy.liu.se/en/student/kurser/TSTE14/	
Result:	Available 2017-06-22	

- 1**
- a. What is the difference between passive and active components and filters?(2 p)
 - b. What is the potential disadvantage of using frequency transformations when synthesizing bandpass and bandstop filters? (2 p)
 - c. Why do doubly resistively terminated LC-filters have lower sensitivity than singly terminated LC filters? (2 p)
 - d. What is characteristic for the frequency response of a distributed-element filter, as opposed to a lumped-element filter? (2 p)
 - e. What is an inverting amplifier? How can it be realized using an OP amplifier and resistors? (2 p)
- 2** Synthesize a Chebyshev-I filter that meets the following specification: $\omega_c = 2\pi \times 120$ krad/s, $\omega_s = 2\pi \times 40$ krad/s, $A_{\max} = 0.5$ dB, and $A_{\min} = 40$ dB. Determine the poles and zeros, and indicate their locations in the s -plane. The filter order should not be higher than necessary. (10 p)
- 3** Realize a Causer filter that meets the following specification: $\omega_c = 2\pi \times 60$ krad/s, $\omega_s = 2\pi \times 300$ krad/s, $A_{\max} = 0.1$ dB ($\rho = 15\%$), and $A_{\min} = 42$ dB. Use a T-type ladder structure. Determine the capacitor and inductor values assuming source and load resistors with the same value according to $R_S = R_L = 50 \Omega$. (10 p)
- 4** Assume two normalized filters with transfer functions as:

$$H_1(s) = \frac{s}{s^2 + 24s + 169}, \quad H_2(s) = -\frac{s}{s^2 + 10s + 169}$$

- a. Compute the poles and zeros of the overall filter $H(s)$ when $H_1(s)$ and $H_2(s)$ are cascade connected, i.e., $H(s) = H_1(s)H_2(s)$. (4 p)
- b. Compute the poles and zeros of the overall filter $H(s)$ when $H_1(s)$ and $H_2(s)$ are parallel connected, i.e., $H(s) = H_1(s) + H_2(s)$. (4 p)
- c. For each of the two cases above, determine $H(j\omega)$ for $\omega = 0$ and $\omega = \infty$ and state the type of filter (lowpass, highpass, bandpass, or bandstop). (2 p)

5 The transfer function of a second-order filter section is given as

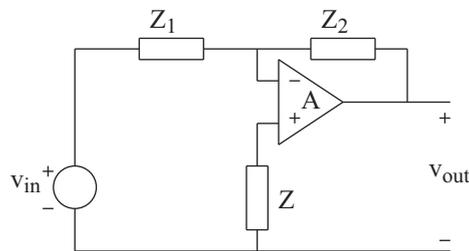
$$H(s) = \frac{G}{s^2 + \frac{r_p}{Q}s + r_p^2}$$

- a. Is this a lowpass, highpass, bandpass, or bandstop filter section? Motivate the answer by sketching the principle behaviour of the magnitude response. (2 p)
- b. Determine the gain constant G so that the magnitude response $|H(j\omega)|$ equals unity at DC (zero-frequency). (1 p)
- c. Express in terms of r_p and Q , the angular frequency ω (say ω_{peak}) at which the magnitude response $|H(j\omega)|$ is maximum. (6 p)
- d. For ω_{peak} to be real-valued, what is the range of values for Q ? (1 p)

- 6
- a. Derive the transfer function $H(s) \triangleq V_{\text{out}}(s)/V_{\text{in}}(s)$ for the active circuit below, expressed in terms of $Z_1(s)$, $Z_2(s)$ and $A(s)$, where $A(s)$ is the transfer characteristics of the OP amplifier. The OP amplifier is thus non-ideal, but its input impedance can be assumed to be infinite in the derivations. (5 p)
 - b. Assume that $Z_2(s)/Z_1(s) = G$, with $Z_1(s)$ and $Z_2(s)$ being real-valued constants, and thus G being a real-valued constant. This means that the circuit is an inverting amplifier. However, due to the non-ideal OP amplifier, $H(s)$ has a lowpass filter frequency response. Determine the 3dB angular frequency for $H(s)$. Use reasonable approximations if necessary. For a lowpass filter $H(s)$, the 3dB angular frequency, say ω_{3dB} , is defined by $|H(j\omega_{3dB})| = |H(j0)|/\sqrt{2}$. Assume that

$$A(s) = \frac{A_0}{1 + \frac{s}{\omega_0}}$$

with $A_0 = 10^5$ and $\omega_0 = 2\pi \times 10$ rad/s. Also assume that $A_0 \gg G$. (5 p)



- 7 Assume that $H(S)$ is a first-order prototype lowpass filter according to

$$H(S) = \frac{G}{S - P}$$

where G is a gain constant and P is the pole, and assume that $H(S)$ is frequency transformed into bandpass and bandstop filters.

- a. Determine the zeros and poles of the bandpass and bandstop filters, expressed in terms of P and the parameter ω_I^2 which is used in the transformations. (6 p)
- b. Assume that we realize the prototype lowpass filter with a first-order π -type ladder structure, and that we transform this realization into the bandpass filter realization. Show that the capacitor in the lowpass filter, with the capacitance C , is transformed into a parallel connection consisting of a capacitor, with the capacitance C , and an inductor, with the inductance $1/(\omega_I^2 C)$. (4 p)