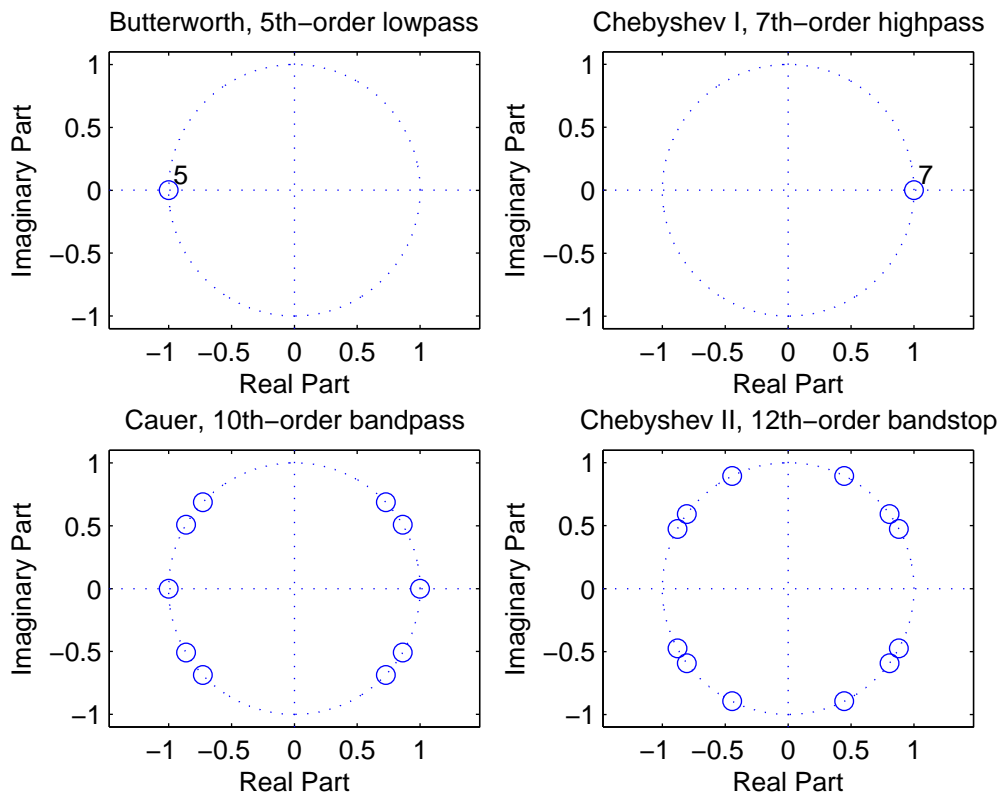


- 1
- a) Lowpass, because  $H(1) = 4$ ,  $H(-1)=0$
  - b) In two's-complementary arithmetics, temporary overflows are okay in partial sums if the final sum is within the number range  $\Rightarrow$  only inputs to noninteger multipliers and the output need to be scaled. Safe scaling: never overflow. Lp-norm scaling: overflow with a certain probability.
  - c) 1) Inserted unit elements between two-ports, propagated into the filter using Kuroda's identities. 2) Directly interconnected adaptors with reflection-free ports.
  - d) The group delay is  $10T$  seconds (10 samples).
  - e)



- 2) Band edges:  $\omega_c T_{\text{sample}} = 0.5 \pi$ ,  $\omega_s T_{\text{sample}} = 0.84559 \pi$ .

Bilinear transform  $\Rightarrow \omega_{ac} = 1$ ,  $\omega_{as} = 4.0417$ .

Requirements on  $\omega_{ac}$ ,  $\omega_{as}$ , and  $A_{\text{min}} \Rightarrow 15 \leq \Theta \leq 15$ .

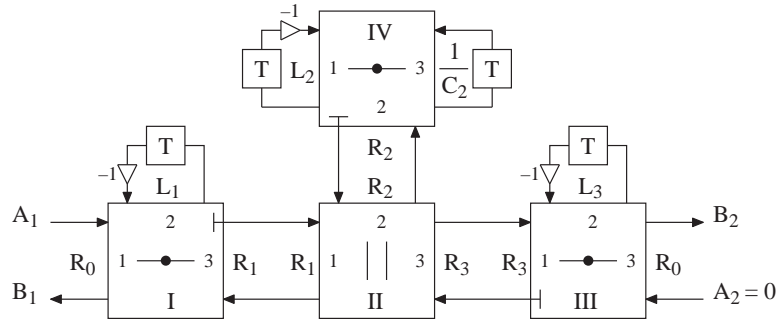
Normalized element values

$$L'_1 = L'_3 = 0.9944, L'_2 = 0.0463, C'_2 = 1.0941$$

Denormalize with  $R_0 = 1$ ,  $\omega_0 = \omega_{ac} = 1 \Rightarrow$

$$L_1 = L_3 = 0.9944, L_2 = 0.0463, C_2 = 1.0941$$

Wave flow graph



Adaptor coefficients:

$$\begin{aligned}
 R_1 &= L_1 + R_0 = 1.9944 & R_3 &= L_3 + R_0 = 1.9944 \\
 \text{I: } \alpha_1 &= \frac{2R_0}{R_0 + L_1 + R_1} = 0.5014 & \alpha_1 &= 1 \\
 \alpha_2 &= 1 - \alpha_1 = 0.4986 & \text{, III: } \alpha_2 &= \frac{2L_3}{R_3 + L_3 + R_0} = 0.4986 \\
 \alpha_3 &= 1 & \alpha_3 &= 1 - \alpha_2 = 0.5014 \\
 \\ 
 R_2 &= L_2 + \frac{1}{C_2} = 0.9603 & \alpha_1 &= \frac{\frac{2}{R_1}}{\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3}} = 0.49057 \\
 \text{IV: } \alpha_1 &= \frac{2L_2}{L_2 + R_2 + \frac{1}{C_2}} = 0.039618 & \text{, II: } \alpha_2 &= \frac{\frac{2}{R_2}}{\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3}} = 1.0189 \\
 \alpha_2 &= 1 & \alpha_3 &= 1 - \alpha_1 - \alpha_2 = 0.49057 \\
 \alpha_3 &= 1 - \alpha_1 = 0.60382 & & 
 \end{aligned}$$

3) Requirements for analog HP filter:

$$\omega_{ac} = \frac{2}{T} \tan\left(\frac{\omega_c T}{2}\right) = \frac{2}{T} \tan(0,325\pi) \approx \frac{2}{T}(1, 631852)$$

$$\omega_{as} = \frac{2}{T} \tan\left(\frac{\omega_s T}{2}\right) = \frac{2}{T} \tan(0,2\pi) = \frac{2}{T}(0, 726542)$$

Requirements for analog LP prototype filter:

$$\Omega_c = \frac{\omega_I^2}{\omega_{ac}} \quad \Omega_s = \frac{\omega_I^2}{\omega_{as}}$$

Choose  $\Omega_c = 1 \Rightarrow$

$$\omega_I^2 = \omega_{ac} \quad \Omega_s = \frac{\omega_{ac}}{\omega_{as}} \approx 2,24605$$

Order: nomogram  $\Rightarrow N = 4$

Normalized poles:

$$S'_{1,2} = -0,1395360 \pm j0,9833792$$

$$S'_{3,4} = -0,3368697 \pm j0,4073290$$

Zeros: 4 at  $S = \text{infinity}$

Denormalize with  $\Omega_c = 1 \Rightarrow S_i = S'_i$

$$\text{LP} \rightarrow \text{HP}: S = \frac{\omega_I^2}{s}$$

Poles:

$$s_{1,2} = \frac{2}{T}(-0.2308 \pm j1.6267)$$

$$s_{3,4} = \frac{2}{T}(-1.96752 \pm j2.37905)$$

Zeros: 4 at  $s = 0$

Transform to digital filter

$$z = \frac{1 + \frac{sT}{2}}{1 - \frac{sT}{2}}$$

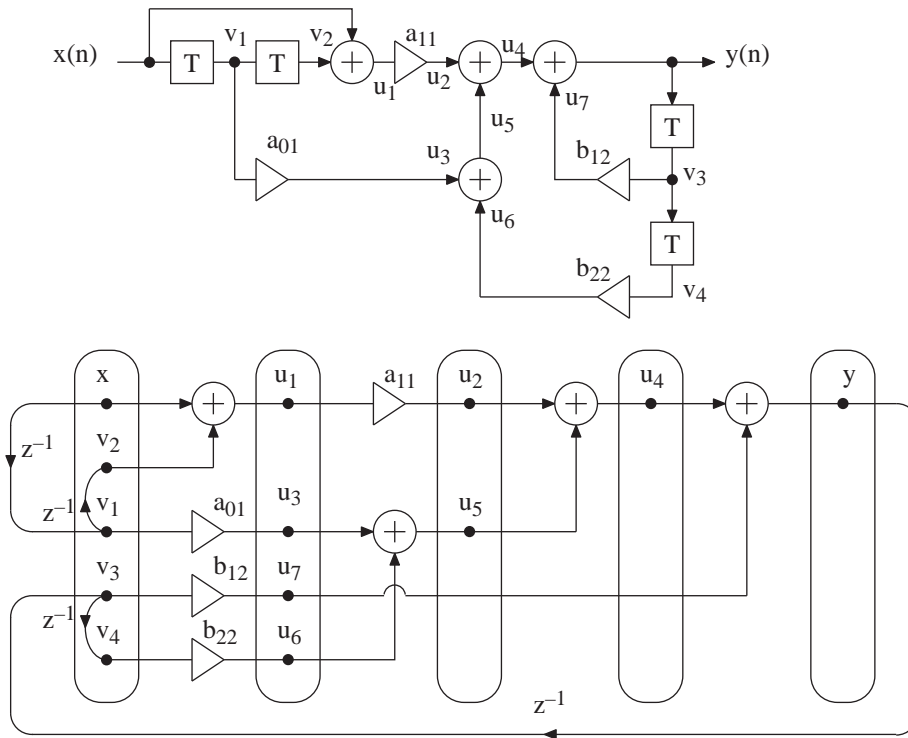
Poles:

$$z_{1,2} = -0.4084 \pm j0.781869$$

$$z_{3,4} = -0.589725 \pm j0.328915$$

Zeros: 4 at  $z = 1$ .

4 a)



b)

$$\begin{aligned}
 u_1 &= v_2 + x & u_7 &= u_4 + u_5 \\
 u_3 &= a_{01}v_1 & y &= u_4 + u_7 \\
 u_7 &= b_{12}v_3 & v_2 &= v_1 \\
 u_6 &= b_{22}v_4 & v_1 &= x \\
 u_2 &= a_{11}u_1 & v_4 &= v_3 \\
 u_5 &= u_3 + u_6 & v_3 &= y \\
 u_4 &= u_2 + u_5 & &
 \end{aligned}$$

c)  $T_{\min} = T_{\text{mult}} + T_{\text{add}} = 1.1 \mu\text{s}$ ,  $T_{\text{CP}} = T_{\text{mult}} + 3T_{\text{add}} = 1.3 \mu\text{s}$

5 a)  $\sigma^2 = 2 \frac{Q^2}{12} \sum_{n=0}^{\infty} h_1^2(n)$

$$H_1(z) = \frac{1}{1 - b_1 z^{-1}} \Leftrightarrow h_1(n) = b_1^n u(n)$$

where  $b_1 = 0.875$

$$\sum_{n=0}^{\infty} h_1^2(n) = \sum_{n=0}^{\infty} b_1^{2n} = \frac{1}{1 - b_1^2}$$

$$\sigma^2 = 2 \frac{Q^2}{12} \frac{1}{1-b_1^2} = 2 \frac{2^{-28}}{12} \frac{1}{1-0,875^2} \approx 2,65 \cdot 10^{-9}$$

b)  $y(n)$  scaled by multiplying  $a_0$  and  $a_2$  by  $c$ .

$$c = \frac{1}{\sqrt{\sum_{n=0}^{\infty} h^2(n)}}$$

$$H(z) = \frac{a_0 + a_2 z^{-2}}{1 - b_1 z^{-1}} \Leftrightarrow h(n) = a_0 b_1^n u(n) + a_2 b_1^{n-2} u(n-2)$$

where  $a_0 = 1, a_2 = -0.25, b_1 = 0.875$

$$h(n) = \begin{cases} 0, & n < 0 \\ a_0, & n = 0 \\ a_0 b_1, & n = 1 \\ \left(a_0 + \frac{a_2}{b_1^2}\right) b_1^n, & n > 1 \end{cases}$$

$$\begin{aligned} \sum_{n=0}^{\infty} h^2(n) &= a_0^2 + (a_0 b_1)^2 + \left(a_0 + \frac{a_2}{b_1^2}\right)^2 \sum_{n=2}^{\infty} b_1^{2n} \\ &= a_0^2 + (a_0 b_1)^2 + \left(a_0 + \frac{a_2}{b_1^2}\right)^2 \frac{b_1^4}{1-b_1^2} = 2,9 \end{aligned}$$

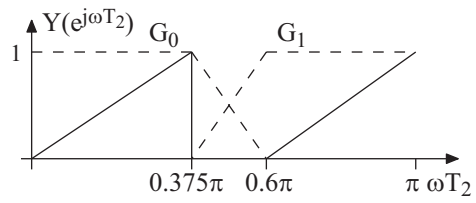
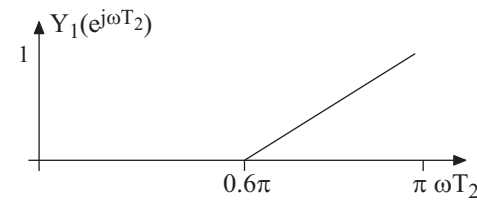
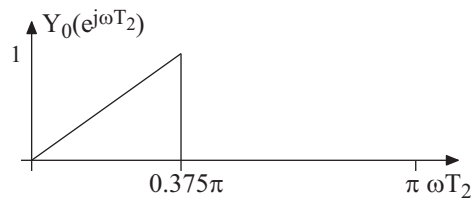
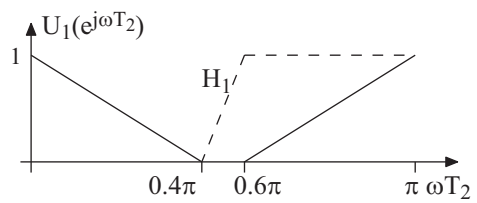
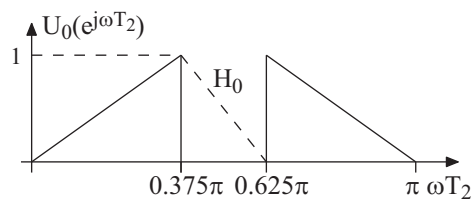
6 a) The passband of the lowpass filter  $G(z)$  is centred around  $2\pi k, k$  integer. Replacing  $z$  with  $z^M$  means that  $2\pi k/M$  must be centred around  $\pi/2$  for an overall highpass filter. Hence,  $M = 4k$ .

$$b) \omega_c^G T = M(\omega_{c2}^H T - \pi/2), \quad \omega_s^G T = M(\omega_{s2}^H T - \pi/2)$$

$$\omega_{c1}^F T = \omega_{c1}^H T, \quad \omega_{c2}^F T = \omega_{c2}^H T$$

$$\omega_{s1}^F T = \omega_{s2}^H T - 2\pi/M, \quad \omega_s^F T = \pi + 2\pi/M - \omega_s^H T$$

7)



$$V_k(e^{j\omega T_2}) = Y_k(e^{j\omega T_2})$$

$$W_k(e^{j\omega T_1}) = X_k(e^{j\omega T_1})$$